CHAPTER 1

Introduction to Geometric Dimensioning and Tolerancing

For many in the manufacturing sector, geometric dimensioning and tolerancing (GD&T) is a new subject. During World War II, the United States manufactured and shipped spare parts overseas for the war effort. Many of these parts, even though they were made to specifications, would not assemble. The military recognized that defective parts caused serious problems for military personnel. After the war, a committee representing government, industry, and education spent considerable time and effort investigating this defective parts problem; this group needed to find a way to ensure that parts would fit and function properly every time. The result was the development of GD&T.

Ultimately, the USASI Y14.5–1966 (United States of America Standards Institute, predecessor to the American National Standards Institute) document was produced based on earlier standards and industry practices. The following are revisions to that standard:

• ANSI Y14.5–1973 (American National Standards Institute)
• ANSI Y14.5M–1982
• ASME Y14.5M–1994 (American Society of Mechanical Engineers)
• ASME Y14.5–2009
• ASME Y14.5–2018

The 2018 revision is the current, authoritative reference document that specifies the proper application of GD&T.

Most government contractors are now required to generate drawings that are tolerated with GD&T. Because of tighter tolerancing requirements, shorter time to production, and the need to communicate design intent more accurately, many companies other than military suppliers are recognizing the importance of tolerancing their drawings with GD&T.

Traditional tolerancing methods have been in use since the mid-1800s. These methods do a good job of dimensioning and tolerancing the size of features and are still used in that capacity today, but they do a poor job of locating and orienting features of size. GD&T is used extensively for tolerancing size, shape, form, orientation, and location of features. Tolerancing with GD&T has a number of advantages over conventional tolerancing methods; three dramatic advantages are illustrated in this chapter.

The purpose of this introductory chapter is to provide an understanding of what GD&T is and why it was developed, when to use it, and what advantages it has over conventional tolerancing methods. With a knowledge of this subject, technical practitioners will be
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more likely to understand tolerancing in general. With this new skill, engineers will have a greater understanding of how parts assemble, do a better job of communicating design requirements, and ultimately be able to make a greater contribution to their companies’ bottom line.

Chapter Objectives

After completing this chapter, the learner will be able to:

- Define GD&T
- Explain when to use GD&T
- Identify three advantages of GD&T over coordinate tolerancing

What Is GD&T?

GD&T is a symbolic language. It is used to specify the size, shape, form, orientation, and location of features on a part. Features toleranced with GD&T reflect the actual relationship between mating parts. Drawings with properly applied geometric tolerancing provide the best opportunity for uniform interpretation and cost-effective assembly. GD&T was created to ensure the proper assembly of mating parts, to improve quality, and to reduce cost.

GD&T is a design tool. Before designers can apply geometric tolerancing properly, they must carefully consider the fit and function of each feature of every part. GD&T, in effect, serves as a checklist to remind the designer to consider all aspects of each feature. GD&T allows the designer to specify the maximum available tolerance and, consequently, design the most economical parts.

Properly applied geometric dimensioning and tolerancing ensures that every part will assemble every time.

GD&T communicates design requirements. This tolerancing scheme identifies all applicable datum features, that is, reference surfaces, and the features being controlled to these datum features. A properly tolerated drawing not only is a picture that communicates the shape and size of the part but also tells a story that explains the tolerance relationships between features.

When Should GD&T Be Used?

Many designers ask, when should I use GD&T? Because GD&T was designed to position features of size, the simplest answer is to locate all features of size with GD&T controls. Designers should tolerance parts with GD&T when:

- Drawing delineation and interpretation need to be the same
- Features are critical to function or interchangeability
- It is important to stop scrapping perfectly good parts
- It is important to reduce drawing changes
- Automated equipment is used
- Functional gaging is required
- It is important to increase productivity
- Companies want across-the-board savings
Advantages of GD&T over Coordinate Dimensioning and Tolerancing

Since the middle of the nineteenth century, industry has been using the plus or minus tolerancing system for tolerancing drawings. This system has several limitations. The plus or minus tolerancing system generates rectangular tolerance zones. A rectangular tolerance zone, such as the example in Fig. 1-1, is a boundary within which the axis of a feature that is in tolerance must lie. Rectangular tolerance zones do not have a uniform distance from the center to the outer edges. In Fig. 1-1, from left to right and top to bottom, the tolerance is ± .005; across the diagonals, the tolerance is ± .007. Therefore, when designers tolerance features with a plus or minus .005 tolerance, they must tolerance the mating parts to accept a plus or minus .007 tolerance, which exists across the diagonals of the tolerance zones.

With the plus or minus tolerancing system, features of size can be specified only at the regardless of feature size condition. Regardless of feature size means that the location tolerance remains the same, ± .005, no matter what size the feature happens to be within its size tolerance. If a hole, like the one in Fig. 1-1, increases in size, it actually has more location tolerance, but, with the plus or minus tolerancing system, there is no way to capture that additional tolerance.

Datum features are usually not specified where the plus or minus tolerancing system is used. Consequently, machinists and inspectors don’t know which datum features apply or in what order they apply. In Fig. 1-1, measurements are taken from the lower and left sides of the part. The fact that measurements are taken from these sides indicates that they are datum features. However, since these datum features are not specified, they are called implied datum features. Where datum features are implied, the designer has not indicated which datum feature is more important and has not specified whether a third datum feature is included. It would be

Figure 1-1  The traditional plus or minus tolerancing system. The axis of the 3-inch-diameter hole, to be in tolerance, must fall inside of the .010 square tolerance zone.
logical to assume that a third datum feature does exist because the datum reference frame consists of three mutually perpendicular planes, even though a third datum feature is not implied. When locating features with GD&T, there are three important advantages over the coordinate tolerancing system:

- The cylindrical tolerance zone
- The maximum material condition modifier
- Datum features specified in order of precedence

**The Cylindrical Tolerance Zone**

The cylindrical tolerance zone is located and oriented to a specified datum reference frame. In Fig. 1-2, the tolerance zone is oriented perpendicular to datum plane A and located with basic dimensions to datum planes B and C. There are no tolerances directly associated with a basic dimension; consequently, basic dimensions eliminate undesirable tolerance stack-up. Because the cylindrical tolerance zone is established at a basic 90° angle to datum plane A and extends through the entire length of the feature, it easily controls the orientation of the axis.

![Diagram](01_Cogorno_CH01_p001-008.indd)

**Figure 1-2** The cylindrical tolerance zone compared with the rectangular tolerance zone.

Unlike the rectangular tolerance zone, the cylindrical tolerance zone defines a uniform distance from true position, the theoretically perfect center of the hole, to the tolerance zone boundary. When a .014-diameter cylindrical tolerance zone is specified about true position, there is a
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Figure 1-4  The size, size tolerance, and feature control frame for the hole in Fig. 1-2.

The size, size tolerance, and feature control frame for the hole in Fig. 1-2. A cylindrical tolerance zone provides a uniform distance from the axis to the tolerance zone boundary. The size and size tolerance are given by Ø3.000-3.030. LOCATION TOLERANCE: Least Material Condition (LMC) and Maximum Material Condition (MMC). The geometric tolerance specifies that the hole be positioned with a cylindrical tolerance zone of .014 in diameter when the hole is produced at its maximum material condition size. The tolerance zone is oriented perpendicular to datum plane A and located with basic dimensions to datum planes B and C. Since the .014-diameter tolerance is specified with a maximum material condition modifier, circle M, a bonus tolerance is available. As the hole size in Fig. 1-2 departs from maximum tolerance if .007 from true position in all directions. A cylindrical tolerance zone circumscribed about a square tolerance zone, such as the one in Fig. 1-3, has 57% more area than the square tolerance.

The Maximum Material Condition Modifier

The maximum material condition symbol (circle M) in the feature control frame is a modifier. It specifies that as the hole in Fig. 1-2 increases in size, a bonus tolerance is added to the tolerance stated in the feature control frame.

The limit tolerance in Fig. 1-4 indicates that the hole size can be as small as 3.000 (maximum material condition) and as large as 3.030 (least material condition) in diameter. The geometric tolerance specifies that the hole be positioned with a cylindrical tolerance zone of .014 in diameter when the hole is produced at its maximum material condition size. The tolerance zone is oriented perpendicular to datum plane A and located with basic dimensions to datum planes B and C. Since the .014-diameter tolerance is specified with a maximum material condition modifier, circle M, a bonus tolerance is available. As the hole size in Fig. 1-2 departs from maximum tolerance if .007 from true position in all directions. A cylindrical tolerance zone circumscribed about a square tolerance zone, such as the one in Fig. 1-3, has 57% more area than the square tolerance.
material condition toward least material condition, additional location tolerance, called *bonus tolerance*, is allowed in the exact amount of such departure. If the hole specified by the feature control frame in Fig. 1-4 is actually produced at a diameter of 3.020, the total available tolerance is a diameter of .034.

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Actual Mating Envelope    3.020
Minus Maximum Material Condition  -3.000
Bonus Tolerance           .020
Plus Geometric Tolerance   +.014
Total Positional Tolerance .034
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The maximum material condition modifier allows the designer to capture all of the available tolerance.

**Datum Features Specified in Order of Precedence**

Datum features are not usually specified on drawings toleranced with the coordinate dimensioning system. The lower and left edges on the drawing in Fig. 1-5 are implied datum features because the holes are dimensioned from these edges. But which datum feature is more important, and is a third datum plane included in the datum reference frame? A rectangular part such as this is usually placed in a datum reference frame consisting of three mutually perpendicular intersecting planes. When datum features are not specified, machinists and inspectors are forced to make assumptions that could be very costly.

![Figure 1-5](image)

Figure 1-5  A conventional drawing with no datum features specified.

The parts placed in the datum reference frames in Fig. 1-6 shows two interpretations of the drawing in Fig. 1-5. With the traditional method of tolerancing, it is not clear whether the lower edge of the part should be resting against the horizontal surface of the datum reference frame as in Fig. 1-6A or if the left edge of the part should be contacting the vertical surface of the datum reference frame as in Fig. 1-6B.

Manufactured parts are not perfect. It is clear that, when drawings are dimensioned with traditional tolerancing methods, a considerable amount of information is left to the machinists'
and inspectors’ judgment. If a part is to be inspected the same way every time, the drawing must specify how the part is to fit in the datum reference frame. Each datum feature must be specified in the feature control frame in its proper order of precedence.

Summary

• GD&T is a symbolic language used to specify the size, shape, form, orientation, and location of features on a part.
• GD&T was created to ensure the proper assembly of mating parts, to improve quality, and to reduce cost.
• GD&T is a design tool.
• GD&T communicates design requirements.
• This text is based on the standard Dimensioning and Tolerancing ASME Y14.5–2018.
• The cylindrical tolerance zone defines a uniform distance from true position to the tolerance zone boundary.
• The maximum material condition symbol in the feature control frame is a modifier that allows a bonus tolerance.
• All of the datum features must be specified in order of precedence.

Chapter Review

1. __________________________ is the current, authoritative reference document that specifies the proper application of GD&T.

2. GD&T is a symbolic language used to specify the ______________________, ______________________, ______________________, ______________________, and ______________________ of features on a part.

3. Features tolerated with GD&T reflect the ______________________ between mating parts.
4. GD&T was created to ensure the proper assembly of ________________, to improve ________________, and to reduce ________________.

5. Geometric tolerancing allows the maximum available ________________ and, consequently, the most ________________ parts.

6. Plus and minus tolerancing generates a ________________ shaped tolerance zone.

7. ________________ generates a cylindrical shaped tolerance zone to control an axis.

8. If the distance across a square tolerance zone is ± .005, or a total of .010, what is the approximate distance across the diagonal? ________________

9. The ________________ defines a uniform distance from true position to the tolerance zone boundary.

10. Bonus tolerance equals the difference between the actual mating envelope size and the ________________.

11. While processing, a rectangular part usually rests against a ________________ consisting of three mutually perpendicular intersecting planes.